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Current rectification in junctions with spin-split superconductors

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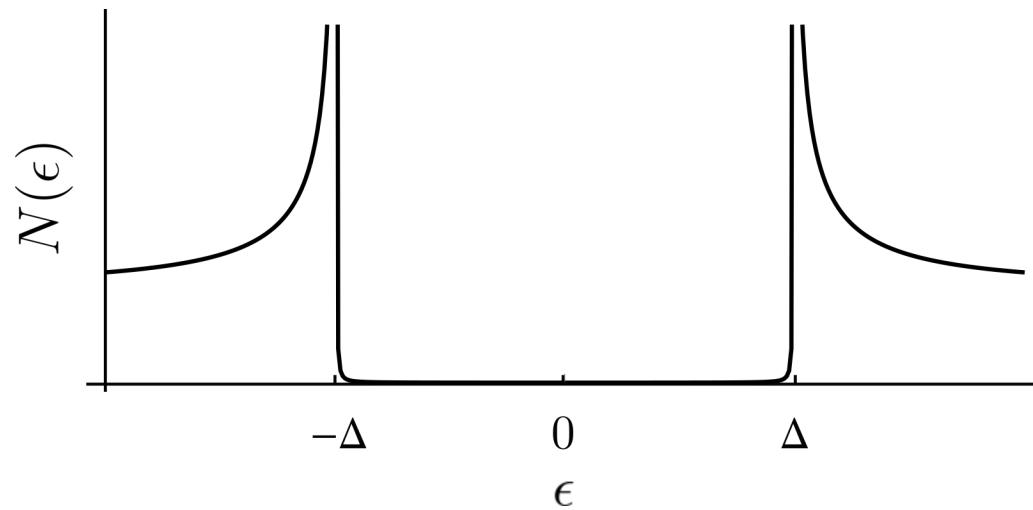
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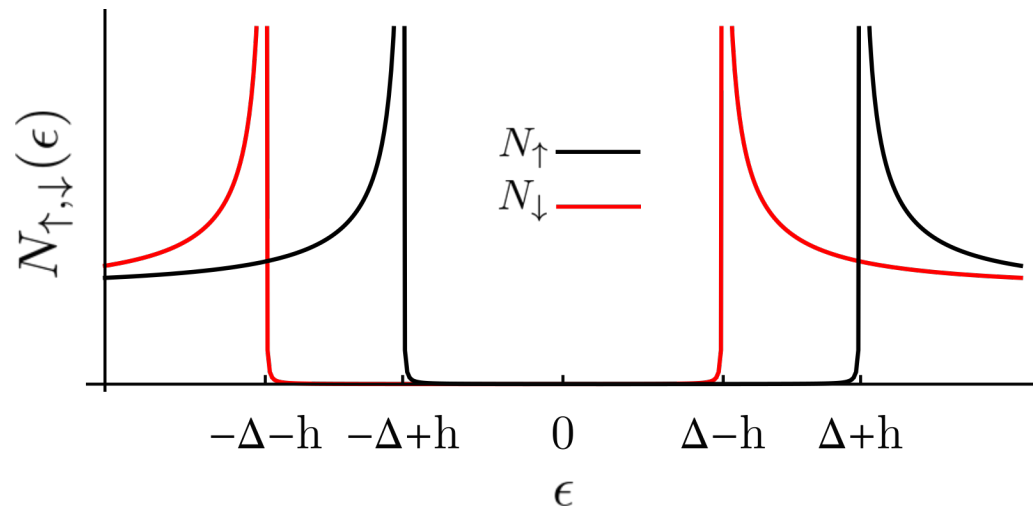
DoS of a superconductor



$$N(\epsilon) = \text{Re} \frac{\epsilon + i\Gamma}{\sqrt{(\epsilon + i\Gamma)^2 - \Delta^2}}$$



Spin-split superconductors

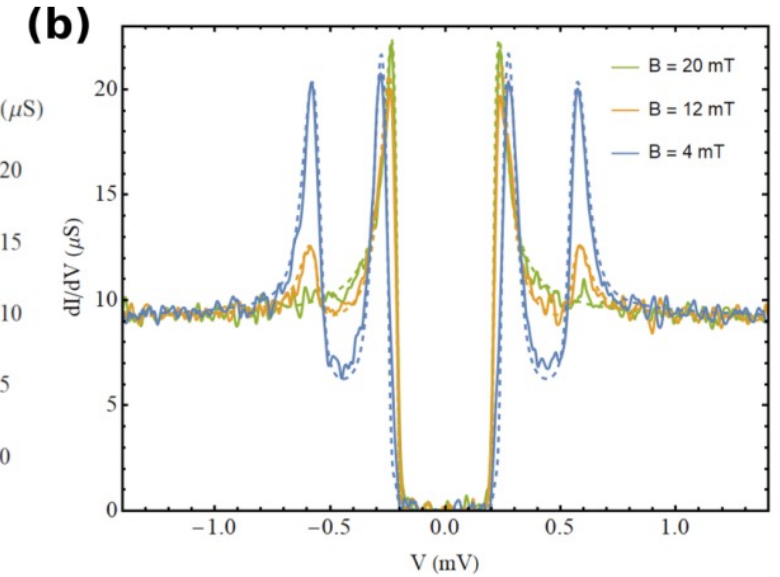
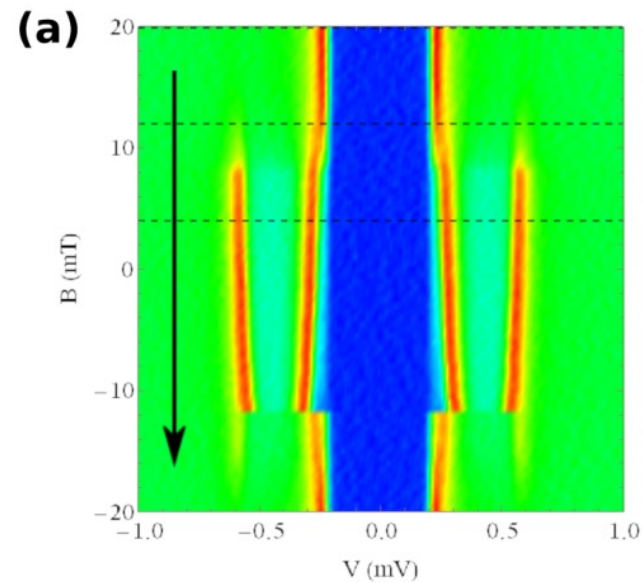
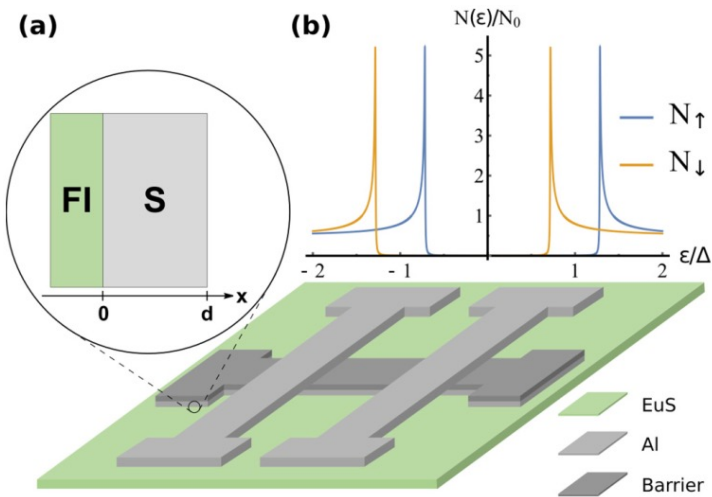


$$N_{\uparrow,\downarrow}(\epsilon) = \text{Re} \frac{\epsilon \pm h + i\Gamma}{\sqrt{(\epsilon \pm h + i\Gamma)^2 - \Delta^2}}$$



Spin splitting in EuS/Al

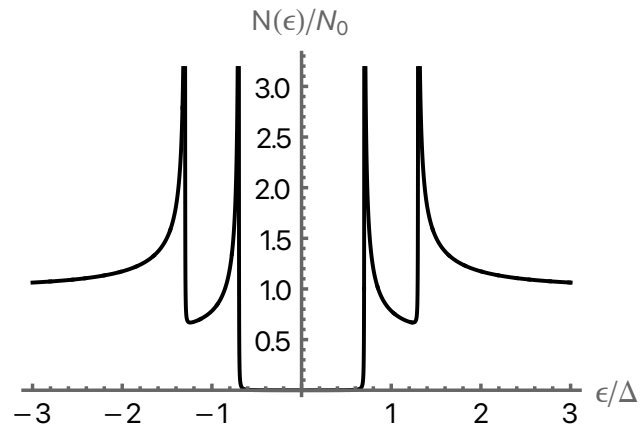
Tunneling conductance in EuS/Al/AIO/Al



Hijano et al, PR Res. 3 (2021)
Moodera et al, PRL 61 (1988)



Spin-filtering and breaking electron-hole symmetry

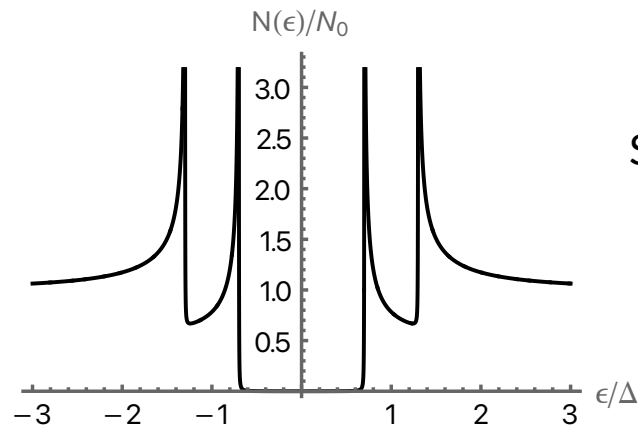


e-h symmetric

$$N(\epsilon) = N(-\epsilon)$$



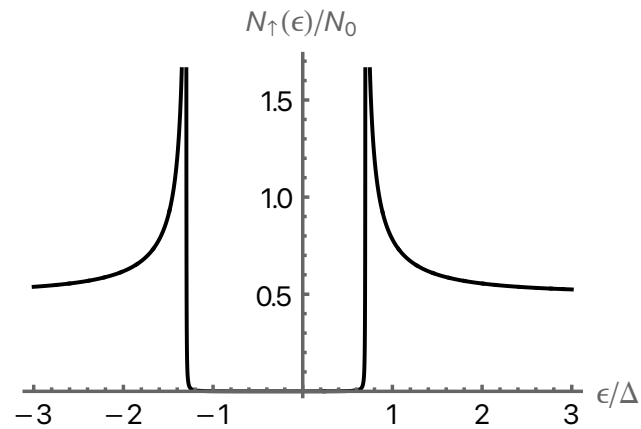
Spin-filtering and breaking electron-hole symmetry



e-h symmetric

$$N(\epsilon) = N(-\epsilon)$$

Spin filtering

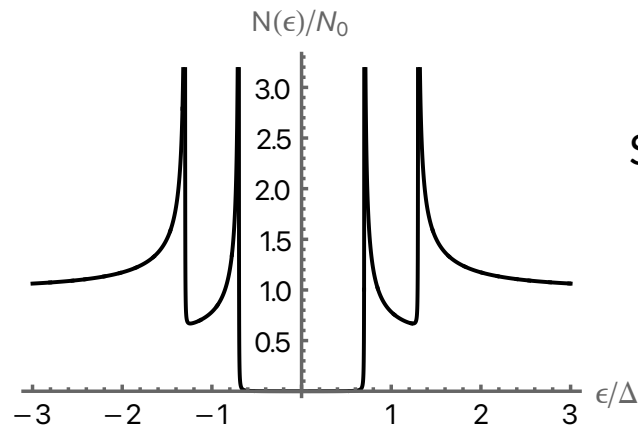


Breaking of e-h symmetry

$$N(\epsilon) \neq N(-\epsilon)$$



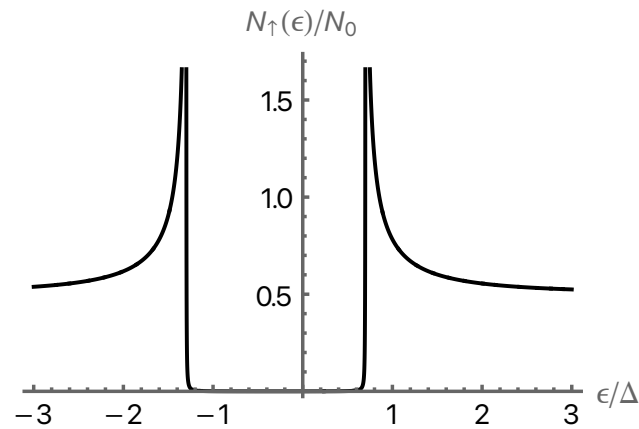
Spin-filtering and breaking electron-hole symmetry



e-h symmetric

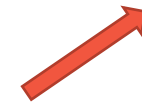
$$N(\epsilon) = N(-\epsilon)$$

Spin filtering



Breaking of e-h symmetry

$$N(\epsilon) \neq N(-\epsilon)$$



Thermoelectric effect
Ozaeta et al, PRL 112 (2014)

Current Rectification
(Diode effect)

Ilic et al, PR Applied 17 (2022)
Strambini et al, Nat. Commun. 13 (2022)

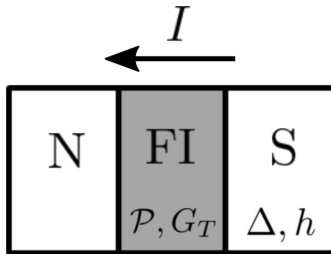


Outline

- DC transport in N/FI/S junctions
 - Thermoelectric effects
 - Current rectification
 - Experimental results
- AC transport in N/FI/S junctions
- Application: radiation detectors



DC transport in N/FI/S tunnel junctions



Spin-split DoS

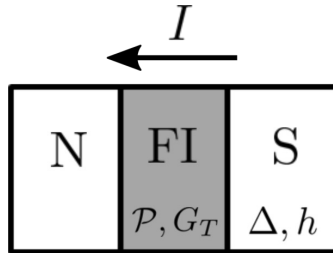
$$N_{\uparrow,\downarrow} = \text{Re} \frac{\epsilon \pm h + i\Gamma}{\sqrt{(\epsilon \pm h + i\Gamma)^2 - \Delta^2}}$$

Spin-polarized tunneling

$$G_{\uparrow} \neq G_{\downarrow}$$



DC transport in N/FI/S tunnel junctions



Spin-split DoS

$$N_{\uparrow,\downarrow} = \text{Re} \frac{\epsilon \pm h + i\Gamma}{\sqrt{(\epsilon \pm h + i\Gamma)^2 - \Delta^2}}$$

Spin-polarized tunneling

$$G_{\uparrow} \neq G_{\downarrow}$$

Charge transport

$$I_{\uparrow,\downarrow} = \frac{G_{\uparrow,\downarrow}}{e} \int d\epsilon N_{\uparrow,\downarrow}(\epsilon) [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

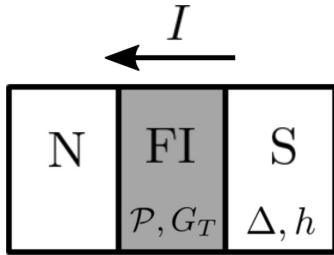
Heat transport

$$\dot{Q}_{\uparrow,\downarrow} = \frac{G_{\uparrow,\downarrow}}{e} \int d\epsilon (\epsilon - eV_{dc}) N_{\uparrow,\downarrow}(\epsilon) [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

$$f_i = \left[1 + e^{\frac{\epsilon}{k_B T_i}} \right]^{-1}$$



DC transport in N/FI/S tunnel junctions



Spin-split DoS

$$N_{\uparrow,\downarrow} = \text{Re} \frac{\epsilon \pm h + i\Gamma}{\sqrt{(\epsilon \pm h + i\Gamma)^2 - \Delta^2}}$$

Spin-polarized tunneling

$$G_{\uparrow} \neq G_{\downarrow}$$

Charge transport

$$I_{\uparrow,\downarrow} = \frac{G_{\uparrow,\downarrow}}{e} \int d\epsilon N_{\uparrow,\downarrow}(\epsilon) [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

Heat transport

$$\dot{Q}_{\uparrow,\downarrow} = \frac{G_{\uparrow,\downarrow}}{e} \int d\epsilon (\epsilon - eV_{dc}) N_{\uparrow,\downarrow}(\epsilon) [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

$$f_i = [1 + e^{\frac{\epsilon}{k_B T_i}}]^{-1}$$

Total currents

$$I = I_{\uparrow} + I_{\downarrow} = \frac{G_T}{e} \int d\epsilon [N_+(\epsilon) + P N_-(\epsilon)] [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

$$\dot{Q} = \dot{Q}_{\uparrow} + \dot{Q}_{\downarrow} = \frac{G_T}{e} \int d\epsilon (\epsilon - eV_{dc}) [N_+(\epsilon) + P N_-(\epsilon)] [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

$$N_{\pm}(\epsilon) = \frac{1}{2} [N_{\uparrow}(\epsilon) \pm N_{\downarrow}(\epsilon)]$$

$$P = (G_{\uparrow} - G_{\downarrow}) / (G_{\uparrow} + G_{\downarrow}) \in [-1, 1]$$



Thermoelectric effects

Expansion for small V_{dc} and $\Delta T = T_S - T_N$

$$\begin{pmatrix} I \\ \dot{Q} \end{pmatrix} = \begin{pmatrix} G & \alpha \\ \alpha & G_{th}T \end{pmatrix} \begin{pmatrix} V_{dc} \\ -\Delta T/T \end{pmatrix}$$

$$G = G_T \int d\epsilon \frac{N_+(\epsilon)}{4 k_B T \cosh^2 \frac{\epsilon}{2 k_B T}}$$

$$G_{th} = \frac{G_T}{e^2} \int d\epsilon \frac{\epsilon^2 N_+(\epsilon)}{4 (k_B T)^2 \cosh^2 \frac{\epsilon}{2 k_B T}}$$

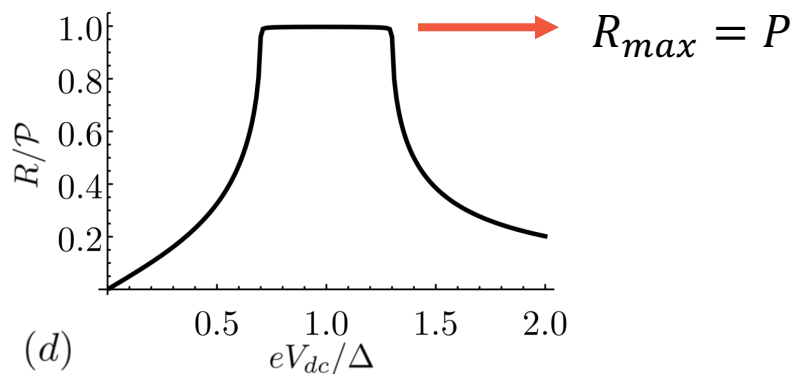
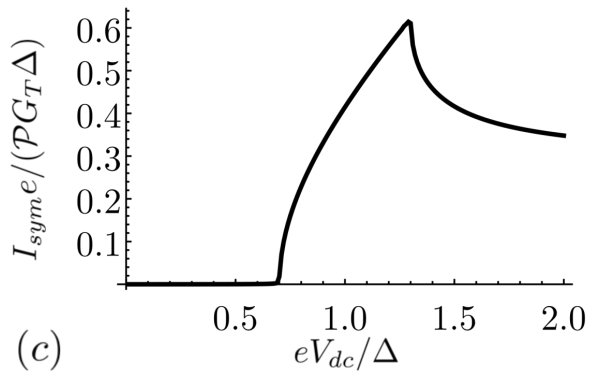
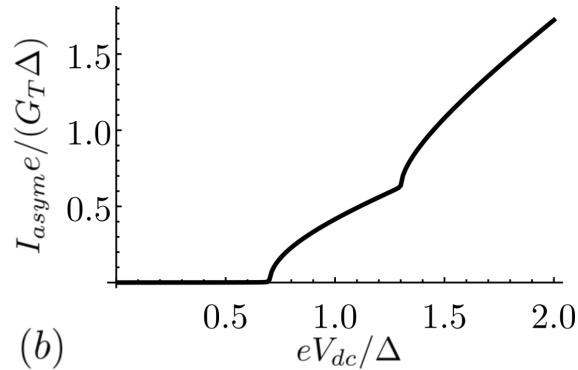
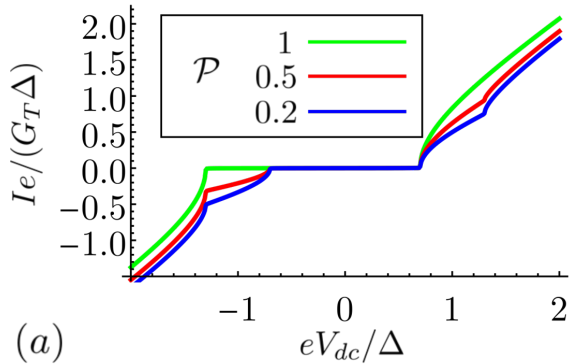
$$\alpha = \frac{G_T}{e} P \int d\epsilon \frac{N_-(\epsilon)}{4 k_B T \cosh^2 \frac{\epsilon}{2 k_B T}}$$



DC current at (near-) zero temperature

$$I = \frac{G_T}{e} \int d\epsilon [N_+(\epsilon) + P N_-(\epsilon)] [f_N(\epsilon - eV_{dc}) - f_S(\epsilon)]$$

$$\frac{\Gamma}{\Delta} \gg \frac{\Delta}{k_B T} e^{-\Delta/k_B T}$$



$I(V) \neq -I(-V) \Rightarrow$ Rectification

$$I_{asym}(V) = \frac{|I(V_{dc}) - I(-V_{dc})|}{2}$$

$$I_{sym}(V) = \frac{|I(V_{dc}) + I(-V_{dc})|}{2}$$

Rectification ratio

$$R = I_{asym}/I_{sym}$$



DC current at finite temperature

$$\frac{\Gamma}{\Delta} \ll \frac{\Delta}{k_B T} e^{-\Delta/k_B T} \quad eV_{dc} < \Delta - h$$

$$I = I_s (e^{eV_{dc}/k_B T} - 1) + I_s (P - 1) \left(\cosh \frac{eV}{k_B T} - 1 \right)$$

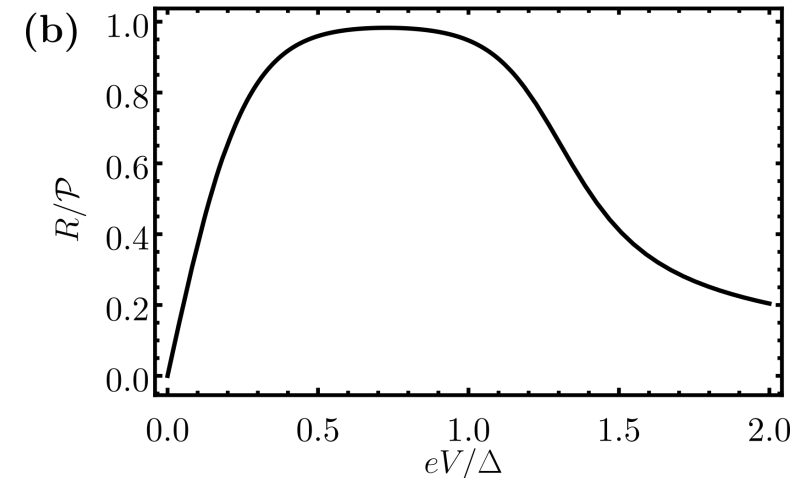
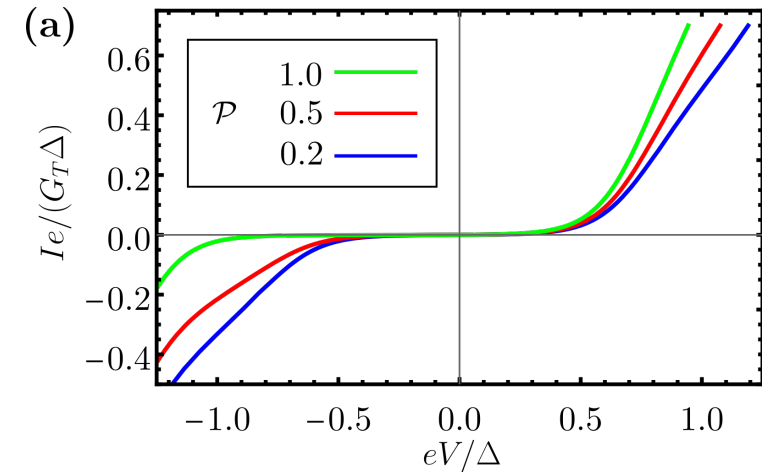


Ideal Schockley
contribution



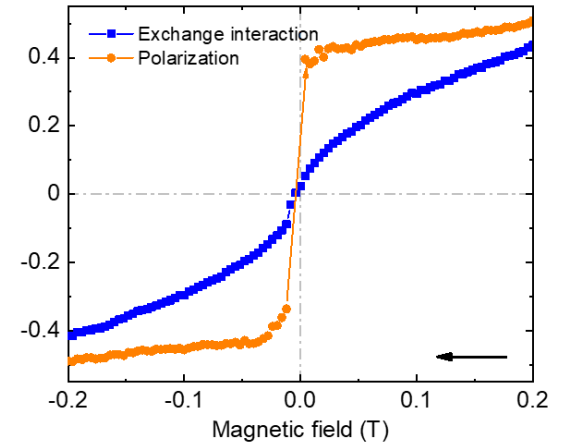
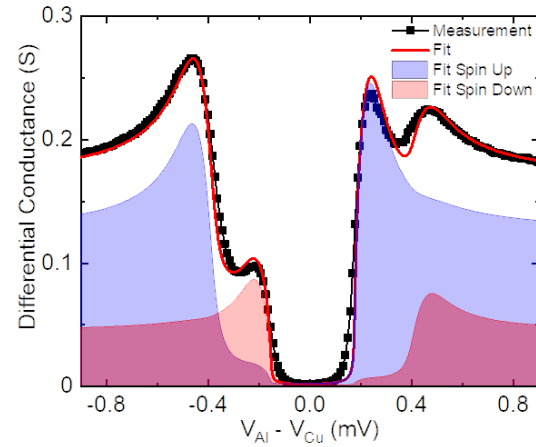
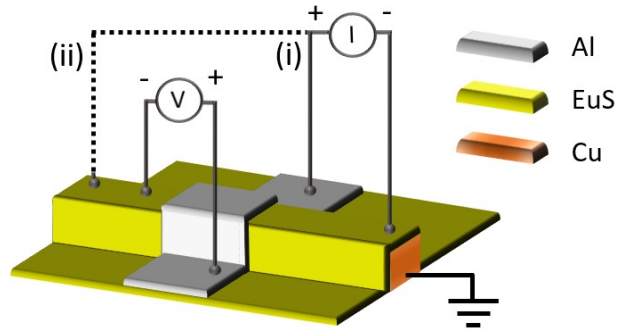
Non-ideality at $P \neq 1$

$$R = \frac{I_{sym}}{I_{asym}} = P \tanh \frac{eV_{dc}}{2 k_B T}$$



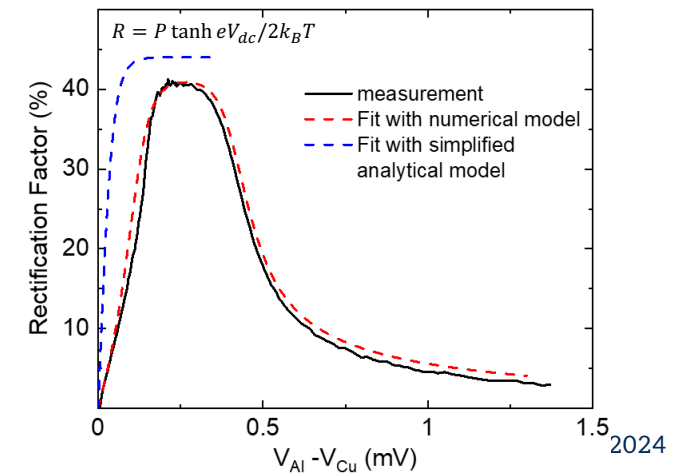
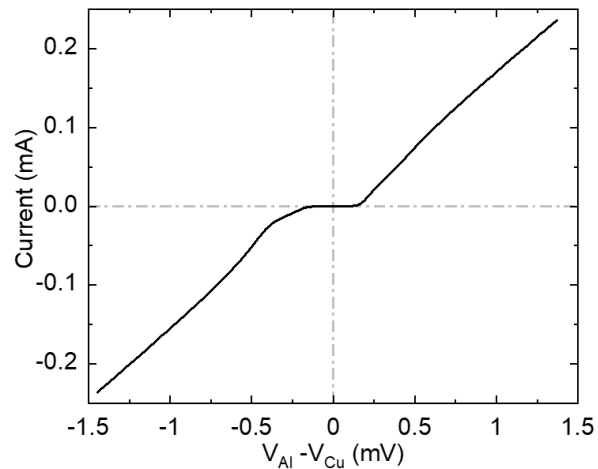
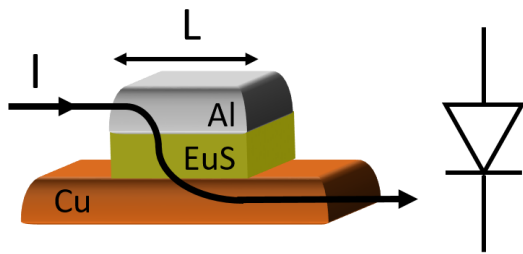
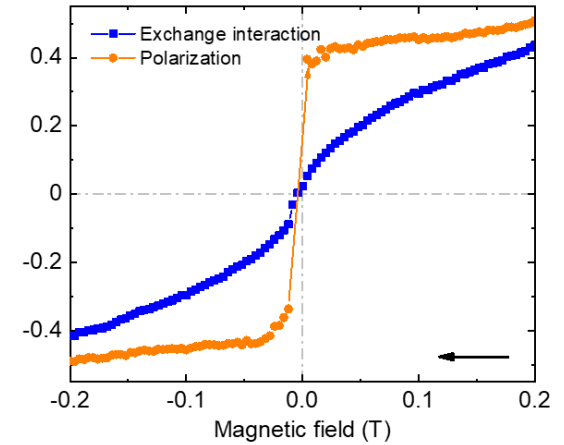
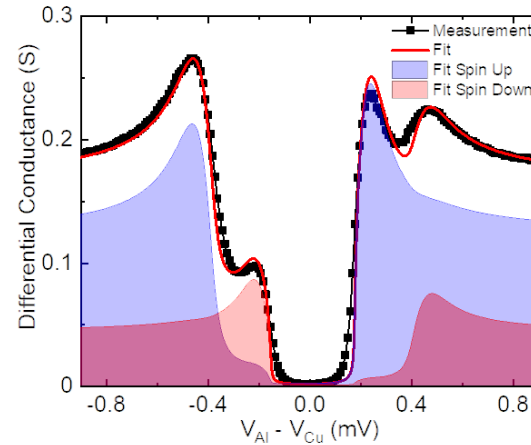
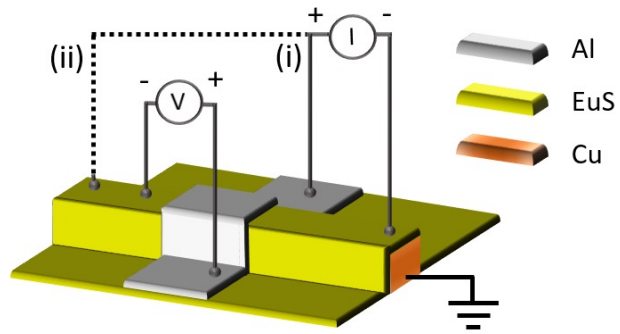


Experimental results in Cu/Al/EuS



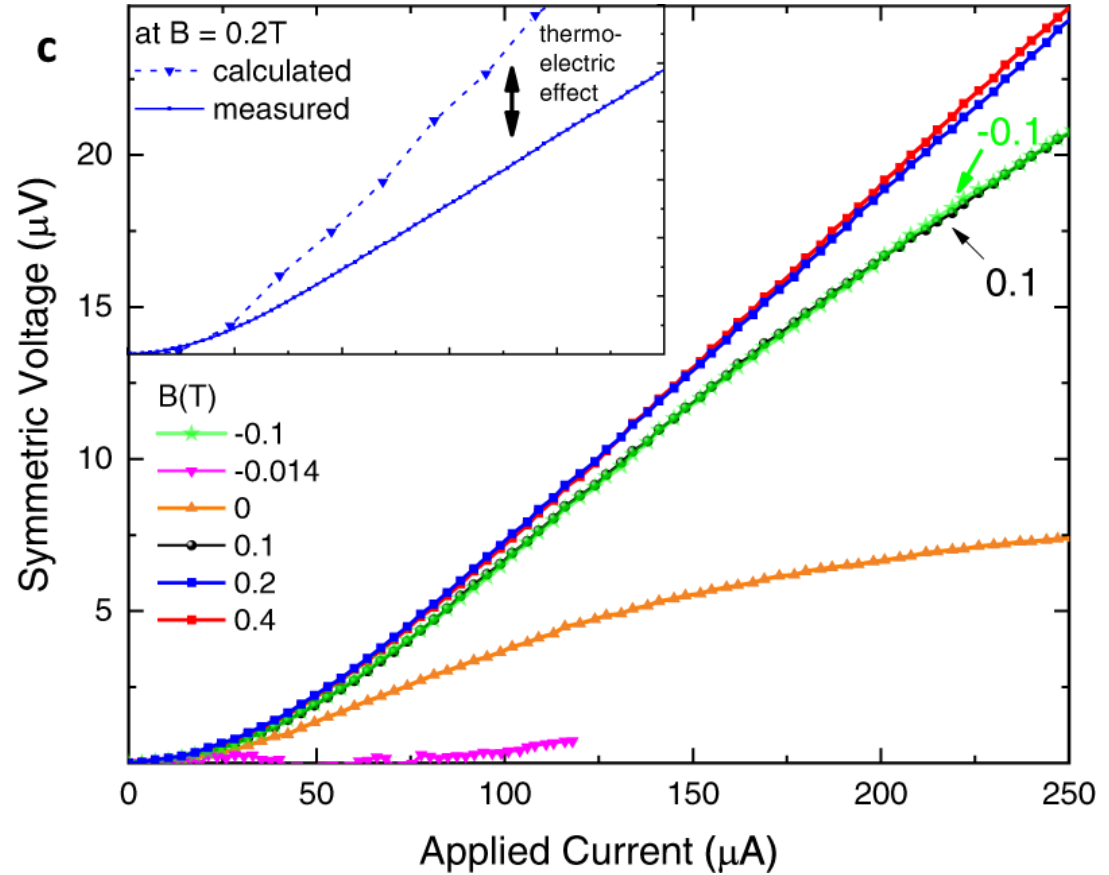
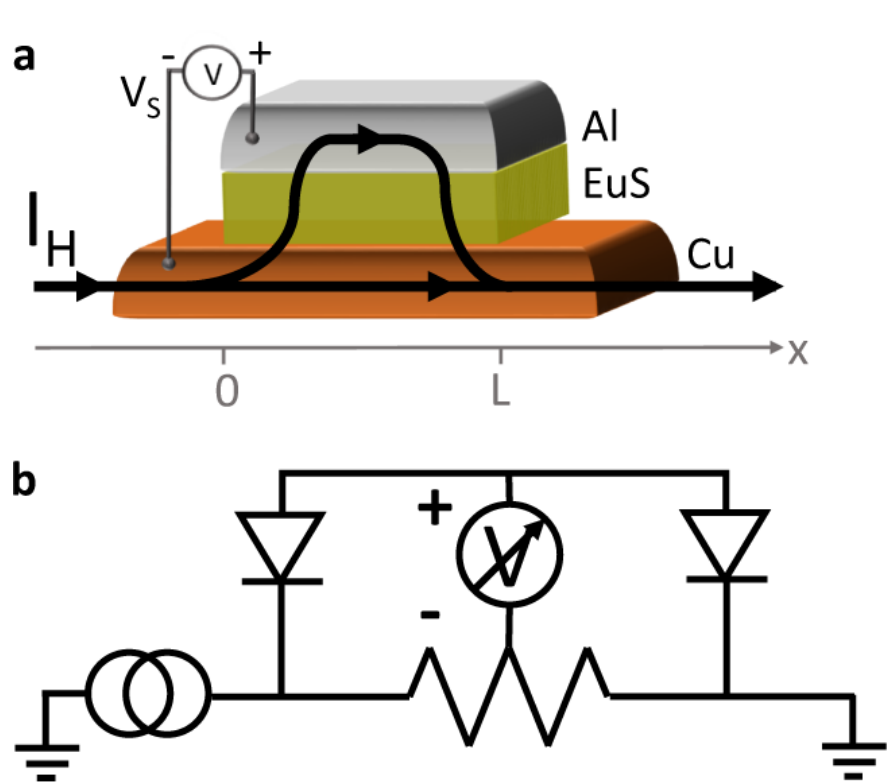


Experimental results in Cu/Al/EuS





Transversal rectifier





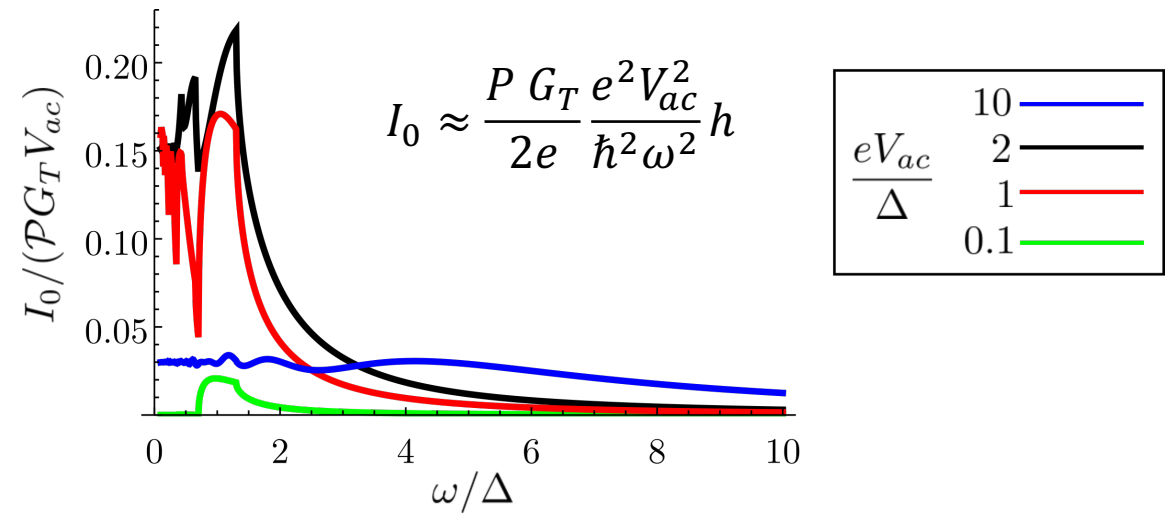
AC current in N/FI/S junctions

$$V(t) = V_{ac} \cos(\omega t)$$

$$I(t) = I_0 + \sum_{m=1}^{\infty} (I_m^c \cos m\omega t + I_m^s \sin m\omega t)$$

$$I_0 = \frac{P G_T}{e} \sum_{n=0}^{\infty} J_n^2 \left(\frac{e V_{ac}}{\hbar \omega} \right) \int d\epsilon N_-(\epsilon) [f_N(\epsilon + n\hbar\omega) - f_S(\epsilon)]$$

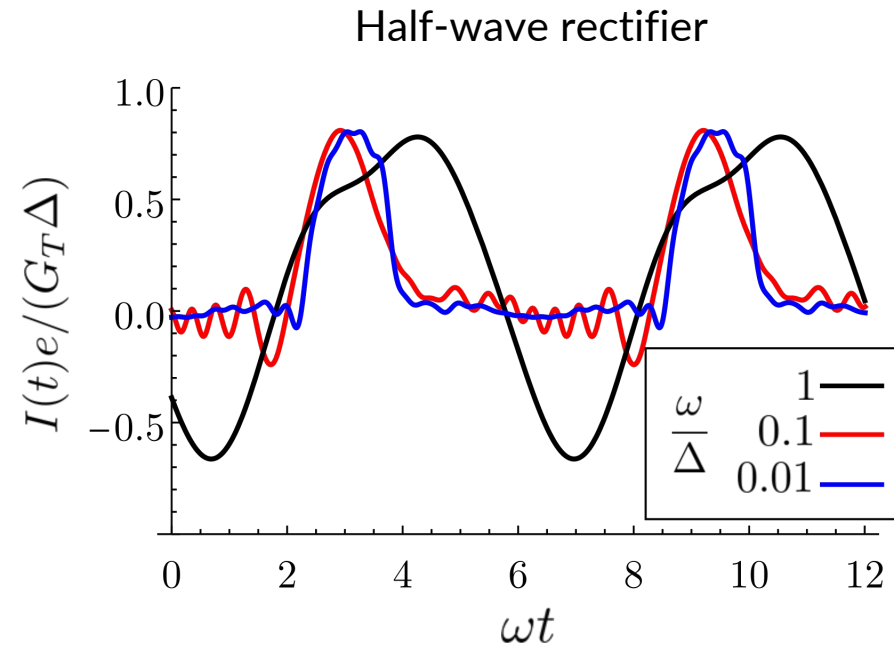
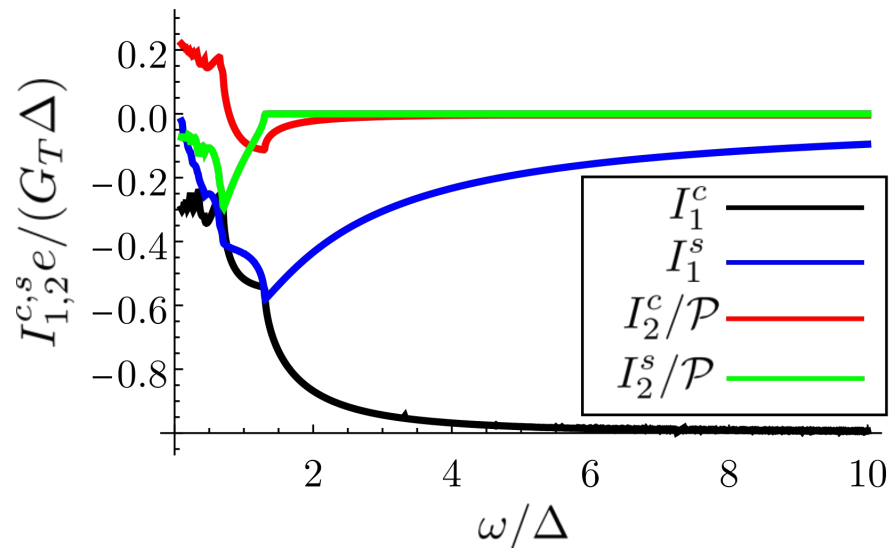
at $\hbar\omega \gg \Delta, k_B T, h, eV_{ac}$





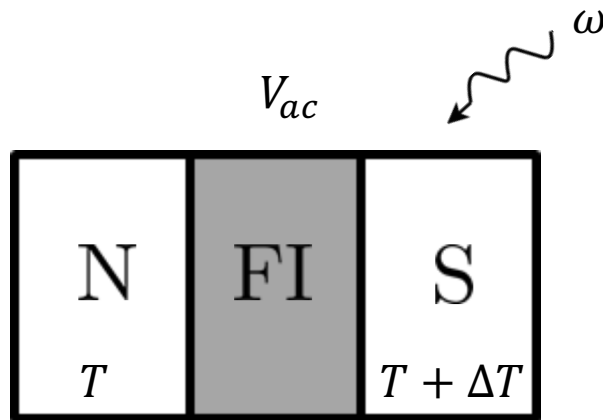
AC current in N/FI/S junctions

$$I(t) = I_0 + \sum_{m=1}^{\infty} (I_m^c \cos m\omega t + I_m^s \sin m\omega t)$$





Application in radiation detectors



$$I = -\alpha \frac{\Delta T}{T} + \frac{P G_T}{2 e} \frac{e^2 V_{ac}^2}{\hbar^2 \omega^2} h$$

- Detected radiation is directly converted into current – self biased detector
- Works at cryogenic temperatures
- Thermoelectricity and rectification compete if $T_s > T_N$ ($\Delta T > 0$), since $\text{sign}(\alpha) = \text{sign}(P h)$
- Heat balance modelling needed to determine ΔT



Detector yield

- Estimate number of generated electrons per photon n at $\hbar\omega \gg \Delta$
- Incoming power $P_\gamma = \hbar\omega/\delta t$

Thermoelectric effect

$$G_{th}\Delta T \propto P_\gamma$$

$$I_{th} = \frac{\alpha\Delta T}{T}$$

$$n_{th} = \frac{I_{th} \delta t}{e} \propto \frac{\alpha \hbar\omega}{e T G_{th}} \approx \frac{P \hbar\omega}{\Delta - h} > 1$$



Detector yield

- Estimate number of generated electrons per photon n at $\hbar\omega > \Delta$
- Incoming power $P_\gamma = \hbar\omega/\delta t$

Thermoelectric effect

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$$I_{th} = \frac{\alpha\Delta T}{T}$$

$$n_{th} = \frac{I_{th} \delta t}{e} \propto \frac{\alpha \hbar\omega}{e T G_{th}} \approx \frac{P \hbar\omega}{\Delta - \hbar} > 1$$

Rectification effect

$$\frac{V_{ac}^2}{2\tilde{R}} \propto P_\gamma \quad \tilde{R} = R/(1 + R G_T)$$

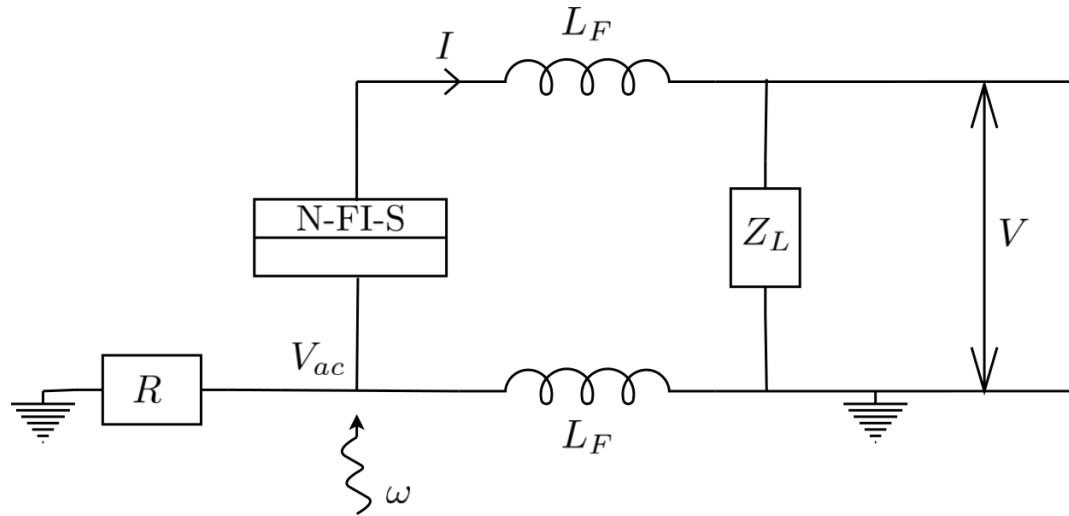
$$I_{rc} \approx \frac{P G_T e^2 V_{ac}^2}{2e \omega^2} h$$

$$n_{rc} = \frac{I_{rc} \delta t}{e} \propto \frac{P \hbar}{\hbar\omega} \tilde{R} G_T < 1$$

- Conclusion: thermoelectric effect contributes more to detection at low temperatures



Radiation detector



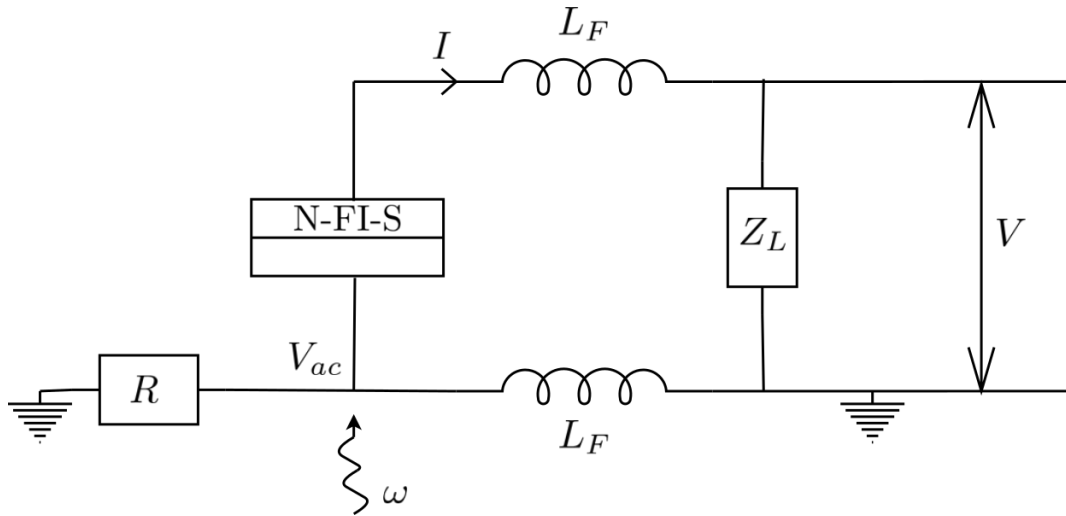
$$NEP = \frac{\sqrt{\langle \delta V^2 \rangle}}{V} P_\gamma$$



Radiation detector

Current

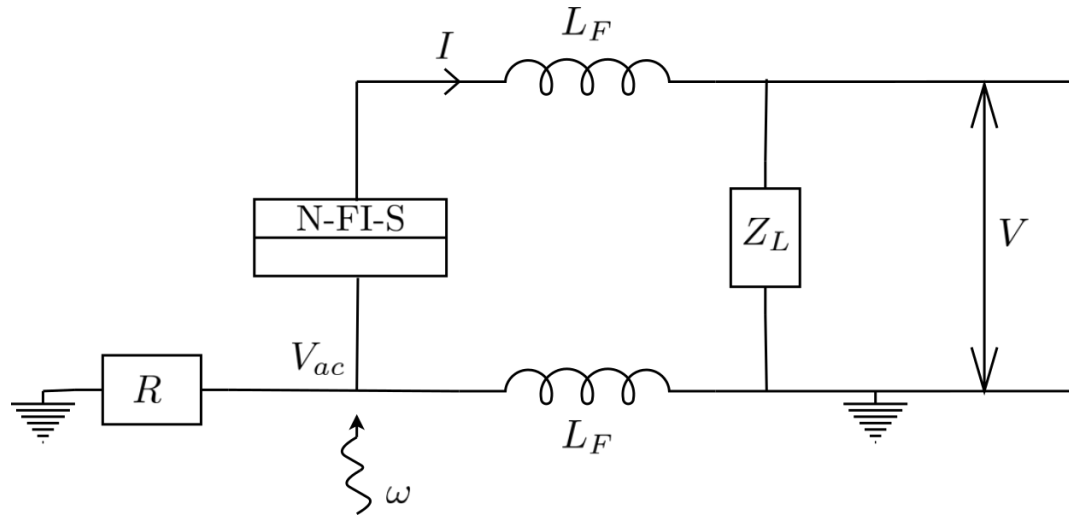
$$I = \alpha \frac{\Delta T}{T} - GV - \frac{P G_T e^2 V_{ac}^2}{2 e \hbar^2 \omega^2} h$$



$$NEP = \frac{\sqrt{\langle \delta V^2 \rangle}}{V} P_\gamma$$



Radiation detector



$$NEP = \frac{\sqrt{\langle \delta V^2 \rangle}}{V} P_\gamma$$

Current

$$I = \alpha \frac{\Delta T}{T} - GV - \frac{P G_T e^2 V_{ac}^2}{2 e \hbar^2 \omega^2} h$$

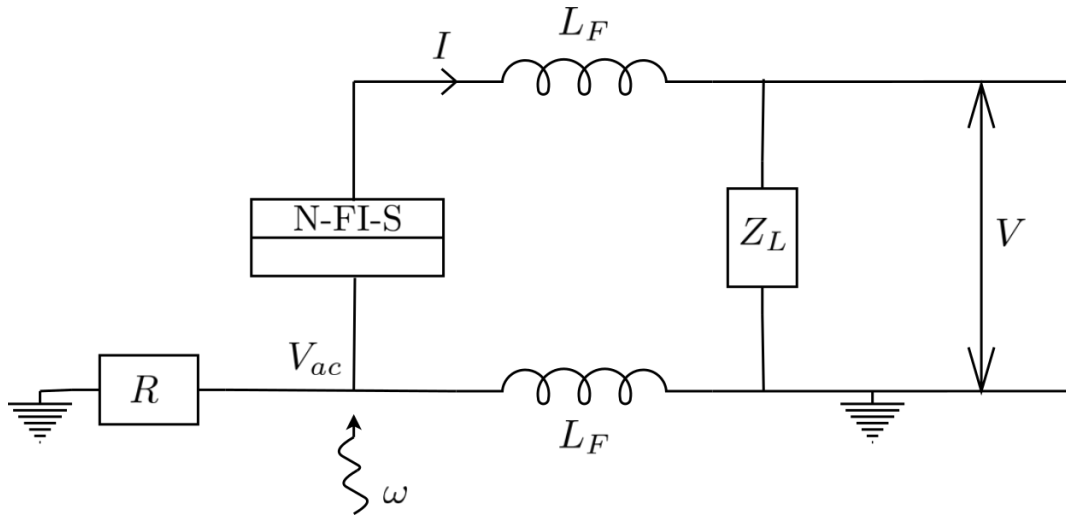
Heat balance

$$P_\gamma = (G_{th} + G_{ph}) \Delta T - \alpha V + \frac{V_{ac}^2}{4} G_T$$

$$G_{ph} = \Sigma \Omega T^4 \Phi(\Delta, h, T)$$



Radiation detector



$$NEP = \frac{\sqrt{\langle \delta V^2 \rangle}}{V} P_\gamma$$

Current

$$I = \alpha \frac{\Delta T}{T} - GV - \frac{P G_T e^2 V_{ac}^2}{2 e \hbar^2 \omega^2} h$$

Heat balance

$$P_\gamma = (G_{th} + G_{ph}) \Delta T - \alpha V + \frac{V_{ac}^2}{4} G_T$$

$$G_{ph} = \Sigma \Omega T^4 \Phi(\Delta, h, T)$$

Noise

$$(G_{th} + G_{ph}) \delta T = \delta \dot{Q}_{ph} + \delta \dot{Q} + \alpha \delta V$$

$$(G + Z_L^{-1}) \delta V = \delta I + \alpha \delta T / T$$

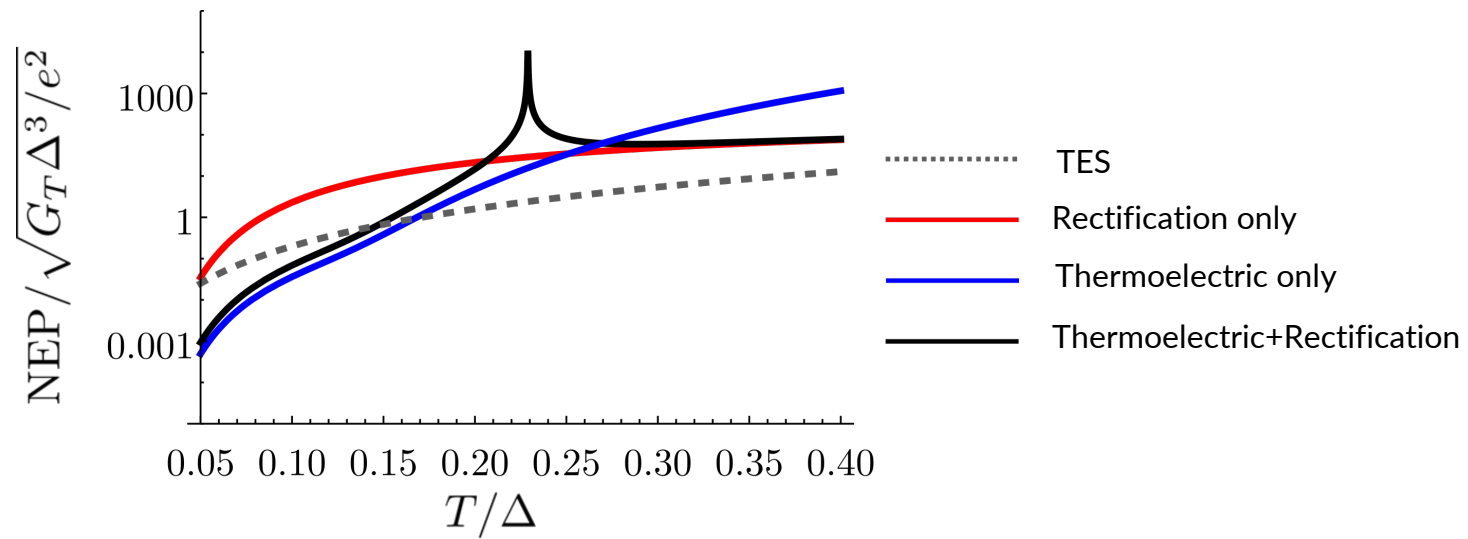
$$\langle \delta I^2 \rangle = 4 k_B T G$$

$$\langle \delta \dot{Q}^2 \rangle = 4 k_B^2 T^2 G_{th}$$

$$\langle \delta I \delta \dot{Q} \rangle = -4 k_B T \alpha$$



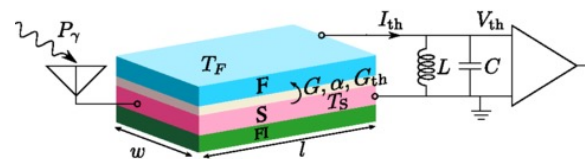
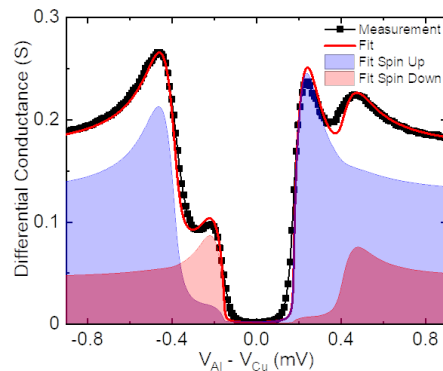
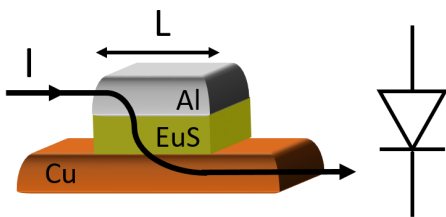
Radiation detector





Summary

- Combination of spin-splitting and spin-filtering in F/S structures breaks electron-hole symmetry
- This enables thermoelectric effects and current rectification
- Applications:
 - Diode for cryogenic electronics
 - Radiation detector
- Review article: Geng et al, Supercond. Sci. Tech. 36 (2023)



We are looking for postdocs!



<https://r.jyu.fi/CondMat>